



Job No: S-123459

Job Title: Building : Bldg1 Revision : 0

Sheet No: 1

Description: Bldg1

Made By: Jack

CK'D By:

Date: 01-Jan-99

BUILDING DATA

 WIDTH = 30.000 (FT)
 LENGTH = 160.00 (FT)
 FRONT EAVE HT... = 8.500 (FT)
 BACK EAVE HT.... = 8.500 (FT)
 PEAK OFFSET = 15.000 (FT)
 FRONT ROOF SLOPE = 0.375 /12

BUILDING CODE DATA

 BUILDING CODE .. = UBC-97
 WIND EXPOSURE .. = C
 SEISMIC ZONE ... =
 DEAD LOAD = 2.000 (PSF)
 COLL LOAD = 0.000 (PSF)
 LIVE LOAD = 30.000 (PSF)
 WIND SPEED = 80.000 (MPH)
 GROUND SNOW = 10.000 (PSF)
 ROOF SNOW = 0.000 (PSF)

DESIGN PRESSURE - P = Ce Cq qs Iw

BASIC VELOCITY PRESSURE - qs = 16.384 (PSF)
 WIND LOAD IMPORTANCE FACTOR - Iw = 1.0
 GUST RESPONSE FACTOR - Ce = 1.060
 INTERNAL PRESSURE COEFF. - GCpi = - 0.5

WIND COEFFICIENTS:

C1 = 0.800 C2 = -0.700 C3 = -0.700 C4 = -0.500

LOAD COMBINATIONS:

1 --> DEAD + LIVE
 2 --> DEAD + WIND

Design of Typ Interior Post

 Dead + Live = 1.814 (kips)
 Dead + Uplift = 0.114 (kips)
 Wind Pressure = 0.000 (klf)
 Lx = 8.469 (ft)
 Ly = 8.469 (ft)
 Kx = 1.000
 Ky = 1.000

SECTION PROPERTIES - 4x2.5 C 16 Ga

Full Cross Section Area (In²) = 0.6
 Eff. Cross Section Area (In²) = 0.43
 Full Section MI @x-x (In⁴) = 1.6
 Full Section MI @y-y (In⁴) = 0.54
 MI for deflection @x-x (In⁴) = 1.46
 Eff. Section Modulus @x-x (In³) = 0.69

1. Compute Nominal Axial Capacity, Pn



Job No: S-123459

Job Title: Building : Bldg1 Revision : 0

Sheet No: 2

Description: Bldg1

Made By: Jack

CK'D By:

Date: 01-Jan-99

$$\begin{aligned} Kx \cdot Lx / rx &= 62.232 \\ Ky \cdot Ly / ry &= 107.122 \\ Fe1 &= 25.393 \text{ ksi (Eq C4.1-1)} \end{aligned}$$

$$\begin{aligned} \text{Sigma ex} &= 75.238 \\ r_o &= 2.907 \\ \text{Beta} &= 0.422 \\ \text{Sigma et} &= 846.437 \\ Fe2 &= 71.433 \text{ ksi (Eq C4.2-1)} \\ \text{Lamda c} &= 1.498 \text{ (Eq C4-4)} \\ Fn &= 84.190 \text{ (Eq C4-2)} \end{aligned}$$

2. Check combined comp. and bending (Sec - C5.2.1)

$$\begin{aligned} \text{Alpha x} &= 0.928 \\ \text{Eq. - 1} &= 0.090 \text{ (Eq C5.2.1-1)} \\ \text{Eq. - 2} &= 0.133 \text{ (Eq C5.2.1-2)} \end{aligned}$$

Design of Typ Exterior Post

$$\begin{aligned} \text{Dead + Live} &= 0.400 \text{ (kips)} \\ \text{Dead + Uplift} &= -0.236 \text{ (kips)} \\ \text{Wind Pressure} &= 0.069 \text{ (klf)} \\ Lx &= 8.000 \text{ (ft)} \\ Ly &= 8.000 \text{ (ft)} \\ Kx &= 1.000 \\ Ky &= 1.000 \end{aligned}$$

SECTION PROPERTIES - 4x2.5 C 16 Ga

$$\begin{aligned} \text{Full Cross Section Area (In}^2) &= 0.6 \\ \text{Eff. Cross Section Area (In}^2) &= 0.43 \\ \text{Full Section MI @x-x (In}^4) &= 1.6 \\ \text{Full Section MI @y-y (In}^4) &= 0.54 \\ \text{MI for deflection @x-x (In}^4) &= 1.46 \\ \text{Eff. Section Modulus @x-x (In}^3) &= 0.69 \end{aligned}$$

1. Compute Nominal Axial Capacity, Pn

$$\begin{aligned} Kx \cdot Lx / rx &= 58.788 \\ Ky \cdot Ly / ry &= 101.193 \\ Fe1 &= 28.456 \text{ ksi (Eq C4.1-1)} \end{aligned}$$

$$\begin{aligned} \text{Sigma ex} &= 84.314 \\ r_o &= 2.907 \\ \text{Beta} &= 0.422 \\ \text{Sigma et} &= 948.535 \\ Fe2 &= 80.049 \text{ ksi (Eq C4.2-1)} \\ \text{Lamda c} &= 1.415 \text{ (Eq C4-4)} \\ Fn &= 75.128 \text{ (Eq C4-2)} \end{aligned}$$

2. Check combined comp. and bending (Sec - C5.2.1)

$$\begin{aligned} \text{Alpha x} &= 0.986 \\ \text{Eq. - 1} &= 0.022 \text{ (Eq C5.2.1-1)} \\ \text{Eq. - 2} &= 0.029 \text{ (Eq C5.2.1-2)} \end{aligned}$$



Job No: S-123459

Job Title: Building : Bldg1 Revision : 0

Sheet No: 3

Description: Bldg1

Made By: Jack

CK'D By:

Date: 01-Jan-99

Design of Typ Jamb Section

 Dead + Live = 0.320 (kips)
 Dead + Uplift = -0.188 (kips)
 Wind Pressure = 0.056 (klf)
 Lx = 8.000 (ft)
 Ly = 8.000 (ft)
 Kx = 1.000
 Ky = 1.000

SECTION PROPERTIES - 4x2.5 C 16 Ga

Full Cross Section Area (In²) = 0.6
 Eff. Cross Section Area (In²) = 0.43
 Full Section MI @x-x (In⁴) = 1.6
 Full Section MI @y-y (In⁴) = 0.54
 MI for deflection @x-x (In⁴) = 1.46
 Eff. Section Modulus @x-x (In³) = 0.69

1. Compute Nominal Axial Capacity, Pn

Kx*Lx/rx = 58.788
 Ky*Ly/ry = 101.193
 Fe1 = 28.456 ksi (Eq C4.1-1)

Sigma ex = 84.314
 ro = 2.907
 Beta = 0.422
 Sigma et = 948.535
 Fe2 = 80.049 ksi (Eq C4.2-1)
 Lamda c = 1.415 (Eq C4-4)
 Fn = 75.128 (Eq C4-2)

2. Check combined comp. and bending (Sec - C5.2.1)

Alpha x = 0.989
 Eq. - 1 = 0.018 (Eq C5.2.1-1)
 Eq. - 2 = 0.024 (Eq C5.2.1-2)

Design of Typ Header Section

 Wind Pressure = 0.056 (klf)
 Lx = 8.000 (ft)
 Ly = 8.000 (ft)
 Kx = 1.000
 Ky = 1.000

SECTION PROPERTIES - 4x2.5 C 16 Ga

Full Cross Section Area (In²) = 0.6
 Eff. Cross Section Area (In²) = 0.43
 Full Section MI @x-x (In⁴) = 1.6
 Full Section MI @y-y (In⁴) = 0.54
 MI for deflection @x-x (In⁴) = 1.46
 Eff. Section Modulus @x-x (In³) = 0.69



Job No: S-123459

Job Title: Building : Bldg1 Revision : 0

Sheet No: 4

Description: Bldg1

Made By: Jack

CK'D By:

Date: 01-Jan-99

1. Compute Nominal Axial Capacity, Pn

$$\begin{aligned} Kx \cdot Lx / rx &= 58.788 \\ Ky \cdot Ly / ry &= 101.193 \\ Fe1 &= 28.456 \text{ ksi (Eq C4.1-1)} \end{aligned}$$

$$\begin{aligned} \text{Sigma ex} &= 84.314 \\ ro &= 2.907 \\ \text{Beta} &= 0.422 \\ \text{Sigma et} &= 948.535 \\ Fe2 &= 80.049 \text{ ksi (Eq C4.2-1)} \\ \text{Lamda c} &= 1.415 \text{ (Eq C4-4)} \\ Fn &= 75.128 \text{ (Eq C4-2)} \end{aligned}$$

2. Check combined comp. and bending (Sec - C5.2.1)

$$\begin{aligned} \text{Alpha x} &= 1.000 \\ \text{Eq. - 1} &= 0.000 \text{ (Eq C5.2.1-1)} \\ \text{Eq. - 2} &= 0.000 \text{ (Eq C5.2.1-2)} \end{aligned}$$

Design of Typ Girt Section

$$\begin{aligned} \text{Wind Pressure} &= 0.022 \text{ (klf)} \\ Lx &= 10.000 \text{ (ft)} \\ Ly &= 1.000 \text{ (ft)} \\ Kx &= 1.000 \\ Ky &= 1.000 \end{aligned}$$

SECTION PROPERTIES - 4x2.5 C 16 Ga

$$\begin{aligned} \text{Full Cross Section Area (In}^2) &= 0.6 \\ \text{Eff. Cross Section Area (In}^2) &= 0.43 \\ \text{Full Section MI @x-x (In}^4) &= 1.6 \\ \text{Full Section MI @y-y (In}^4) &= 0.54 \\ \text{MI for deflection @x-x (In}^4) &= 1.46 \\ \text{Eff. Section Modulus @x-x (In}^3) &= 0.69 \end{aligned}$$

1. Compute Nominal Axial Capacity, Pn

$$\begin{aligned} Kx \cdot Lx / rx &= 73.485 \\ Ky \cdot Ly / ry &= 12.649 \\ Fe1 &= 53.961 \text{ ksi (Eq C4.1-1)} \end{aligned}$$

$$\begin{aligned} \text{Sigma ex} &= 53.961 \\ ro &= 2.907 \\ \text{Beta} &= 0.422 \\ \text{Sigma et} &= 60706.240 \\ Fe2 &= 53.931 \text{ ksi (Eq C4.2-1)} \\ \text{Lamda c} &= 1.028 \text{ (Eq C4-4)} \\ Fn &= 39.641 \text{ (Eq C4-2)} \end{aligned}$$

2. Check combined comp. and bending (Sec - C5.2.1)

$$\begin{aligned} \text{Alpha x} &= 1.000 \\ \text{Eq. - 1} &= 0.000 \text{ (Eq C5.2.1-1)} \\ \text{Eq. - 2} &= 0.000 \text{ (Eq C5.2.1-2)} \end{aligned}$$



Structural DesignSoft, Inc.
5151 S Howell Ave. #F, Milwaukee, WI, 53154
(414) 294-4795

ENGINEERING DEPT.

Job No: S-123459

Job Title: Building : Bldg1 Revision : 0

Sheet No: 5

Description: Bldg1

Made By: Jack

CK'D By:

Date: 01-Jan-99

Diaphragm Bracing

Longitudinal Wind Load = Hor. Design Wind Pressure*Bldg Width*Mean Roof Ht/2.0
= 13.894 psf*30.000 ft*0.000 ft/2.0
= 0.000 kip
Longitudinal Seismic Load = 0.000 kip

Wind Load Governs over Seismic Load

Diaphragm Strength of StormProofPanel 29 Ga Galvalume Plus= 0.100 klf

Required Longitudinal Wall = Longitudinal Load/Diaphragm Strength of Panel
= 0.000 k/0.10 klf
= 0.00 ft

Lateral Wind Load = Hor. Design Wind Pressure*Bldg Length*Mean Roof Ht/2.0
= 13.894 psf*160.000 ft*0.000 ft/2.0
= 0.000 kip

Lateral Seismic Load = 0.000 kip

Wind Load Governs over Seismic Load

Required Lateral Partition Length = Lateral Load/Diaphragm Strength of Panel
= 0.000 k/0.10 klf
= 0.00 ft